



Chemical Vapor Deposition of Coatings On Glass

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Outline

- Materials and Coating Design for Architectural Applications
- Process and Equipment
- Deposition Mechanisms
- Materials and Coating Design for Solar Applications

Needs and wants Characteristics Constraints



Materials and Design for Architectural Applications





- Heat management
- Color / aesthetics



- Visible transmission
 - As high as possible
 - VLT ~ 75% (typ.)
- Heat management for architectural applications
 - Thermal
 - Solar control
- Reflection
 - Codes in many major cities specify <20%





Interactions with Electromagnetic Spectrum



Materials Design – Optical Response

• Fluorine doped SnO₂ (FTO, SnO₂:F)



Emissivity

For an object exposed to a thermal / blackbody source

Absorbed Energy = $\alpha_{\lambda} E_{b\lambda}(\lambda, T)$

Emitted Energy = $\varepsilon_{\lambda} E_{b\lambda}(\lambda, T)$

where ε_{λ} is the emissivity of the object at wavelength λ

Emissivity

At thermal equilibrium

Emitted Energy = *Absorbed Energy*

Leading to $\varepsilon_{\lambda} = \alpha_{\lambda}$ (Kirkoff's law)





Emissivity

The average emissivity then is

$$\bar{\varepsilon} = \frac{\int_0^\infty \varepsilon_\lambda E_{b\lambda}(\lambda, T) \, d\lambda}{\int_0^\infty E_{b\lambda}(\lambda, T) \, d\lambda}$$

Or (invoking Kirkoff's law)

$$\bar{\varepsilon} = \frac{\int_0^\infty \alpha_\lambda E_{b\lambda}(\lambda, T) \, d\lambda}{\int_0^\infty E_{b\lambda}(\lambda, T) \, d\lambda}$$

Where α_{λ} is (reasonably) measurable in the lab



Emissivity of Uncoated Glass



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Emissivity of SnO₂:F Conductive Coating



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Skin Depth (1/e) of Conductive SnO₂:F Coating



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- Emissivity control
 - Coating thickness
 - Doping efficiency



Coating thickness (microns)

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- Growth modes
 - Amorphous layers
 Flat interfaces
 - Crystalline / columnar growth
 - Crystal quality improves with increased thickness
 - Increased surface roughness



Heat transfer mechanisms

- Radiation transport

 thermal regime
 - Parallel surfaces



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Radiative Heat Transfer through glass with and without passive low-e coating



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Windows design for reduced heat transfer

- Heat transfer mechanisms
 - Convection
 - Conduction



Window Design



Heat transfer = $U * A * \Delta T$

Single pane clear glass U = 1.11

Type: Pyrolitic Low-E Clear Insulating Glass *"Sungate[®]"* 500 (2) Clear + Clear by PPG Industries, Inc.

Outdoor Lite: Clear Glass, Pyrolytic Coated on second surface (2) Indoor Lite: Clear Float Glass Low-E Coating: *"Sungate"* 500 (Pyrolitic) by PPG Industries, Inc. Location: Second Surface (2)



Insulating Glass Unit (IGU) window with CVD low-e coating reduces energy loss by 3X as compared with windows with single pane of glass

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Window Design – resources

Publications Softw	are Facilities Site Map Staff Links H					
Choosing a Residential Win	dow Specifying Fenestration Products Questions and Comments					
Windows & daylighting	Software Tools					
► Glazing Materials ► Glazing Materials ► Glazing Materials						
Software	<u>THERM</u> for analyzing two-dimensional heat transfer through build					
Advanced Systems	Optics					
Window Properties	for analyzing optical properties of glazing systems					
Daylighting	International Glazing Database Optical data for glazing products used by WINDOW 5.2 ϵ					
Residential Performance	Complex Glazing Database					
Commercial Performance	database of shading materials and systems, such as rc calculate thermal and optical characteristics of window					

http://windows.lbl.gov/software/

http://www.ppgideascapes.com/Glass/Tools-Resources.aspx

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	Home	/ Glass / Tools &	Technical Resou	rces					

Tools & Technical Resources

PPG is your source for information

PPG Architectural Glass offers a comprehensive set of tools and design resources to help architects, specifiers, fabricators and glaziers identify and work with the PPG glass products that best meet their projects' aesthetic and performance goals.



Tools

Search for glass types, construct IGUs, view glasses in 3-D and compare their energy and thermal stress performance results.



Design Resources

Find and explore information on sustainability, LEED® compliance and Cradle to Cradle^{CM} Certification. View our glass design guidelines and learn more about glass. Then check out our



Architectural Glass Specifications

Find a list of product performance characteristics for all PPG architectural glass products to help you compare and meet your design requirements.

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- Color can be represented in L*a*b* space
 - Weighting functions in visual spectrum give
 - L* brightness
 - a* red/green axis
 - b* yellow/blue axis
- Customers want
 - Neutral ~ (0,0)
 - Blue-green (-a*, -b*)



- Optical response
 - Design of coating stack
 - Response often non-linear in color space







- Optical response
 - Add color suppression layer between high index (SnO2:F) and low index (glass)





Coating Design – Color Suppression Layer

- **Color suppression layer approaches**
 - Discrete H-L index layers
 - + $SnO_2 / SiO_2 / SnO_2 / SiO_2$
 - Homogenous intermediate index layer
 - + $Si_xSn_{(1-x)}O_{(2-\delta)}C_{\delta}$
 - Graded optical index
 - Mixed metal oxides

 - Si_xSn_(1-x)O₂ (x is a function of layer thickness)
 Si_xTi_(1-x)O₂ (x is a function of layer thickness)

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Chemistry for CVD Coatings

- **Typical precursors** All are unsafe if not used properly!
 - SnO₂
 - + Monobutyl tin trichloride ($C_4H_9SnCl_3$)
 - Bibutyl tin dichloride ((CH₃CH₂CH₂CH₂)₂SnCl₂)
 - + Trimethyl tin ($C_4H_{12}Sn$)
 - F
- Hydrofluoric acid (HF)
- + Trifluoroacetic acid ($C_2HF_3O_2$)
- SiO₂
 - Tetraethyl orthosilicate (SiC₈H₂₀O₄ TEOS)
 - ✦ Silane (SiH₄)
 - Monochlorosilane (SiClH₃)
- TiO₂
 - Titanium isopropoxide (C₁₂H₂₈O₄Ti)
 - + Titanium tetrachloride $(TiCI_4)$

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Choosing a precursor – criteria to consider

- Safety
 - Toxic (acute, chronic exposure)
 - Flammable / pyrophoric
 - Asphyxiate (CO₂ vs N₂ vs NF₃)
- Compatibility with other precursors

 $2MCI_3 + 3H_2O \rightarrow 6HCI + MO_x + yO_2$

(~instantaneous, exothermic)

- Deposition efficiency within desired / allowable temperature regime
- Cost



Questions

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Process and Equipment

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Process & Equipment – coater location



- Float glass
 - 25 MM m²/yr per line

- Glass Temperature = 600-675°C
- Glass Speed = 5 to 15 meters/min.

- Online CVD coating
 - 10 MM m²/yr per line
- Efficient use of energy
 - Use existing energy content of the glass

Precursor flow system



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Process & Equipment – precursor vaporization



- Liquid distributor fouling resistance (best to worst)
 - V-notch weir
 - Spray
 - Slotted weir
 - Sidewall orifice
- Packing types
 - Metal chips
 - Raschig rings
 - Pall rings

Process & Equipment – vaporizer operations



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Process & Equipment – vaporizer operation

- What is the operating temperature for vaporization of MBTC
 - 36.5 lb/hr MBTC flow
 - 20 SCFM N₂

 $MW_{MBTC} = 282 \text{ lb / lb-mol}$ $N_2 \text{ std vol} = 386.7 \text{ SCF / lb-mol}$

MBTC concentration = 4%

 $T_{op} > 271 F$

If $T_{op} < 270F$ expect liquid into pot

Condensation temperature (F) of MBTC as a function of vapor phase concentration



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Process & Equipment – vaporizer operation

 Souder-Brown equation predicts entrainment when velocity V in the vaporizer packed column is greater than V_G

Souder-Brown Eqn.

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$$V_G = k \sqrt{\frac{\rho_L - \rho_G}{\rho_G}}$$

For packed column k = 0.175 ft/s

 $\rho_{\text{MBTC}} = 91.95 \text{ lb/ft}^3$ $\rho_{\text{vap}} = 0.0531 \text{ lb/ft}^3$

54.75 lb/hr MBTC 30 SCFM N₂ T=300 F

12 tubes (1-1/4" sch 10) ID = 1.442"

 $V_{vap+chem} = 5.49 \text{ ft/s}$ $V_G = 4.93 \text{ ft/s}$

Entrainment is expected \rightarrow "coater drip"

Process & Equipment – basic coater design

Single inlet and exhaust



Process & Equipment – basic coater design

 Inlet paired with 2 exhausts with flows both upstream & downstream





Flows and temperatures under coater





Deposition mechanism



$$J = \frac{c_g}{\delta/D + 1/k_s}$$

2 mechanisms: (1) mass transport, (2) reaction at surface

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Deposition Mechanism

C

$$J = \frac{c_g}{\delta/D}$$
$$\delta(x) \propto \sqrt{x/u}$$

$$\propto \sqrt{x/u}$$

$$J = C_g k_s = C_g e^{-E/kT}$$
$$T = F(x)$$



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SnO₂ deposition from MBTC

Inlet slot Exhaust Exhaust slot slot 70 experiment 2nd order upwind 60 **9**8-8-8-8₆ **Deposition of SnO**₂ 10 Is transport controlled 0∟ -2.5 -2 -1.5 -0.50.5 1.5 2 2.5 -1 0 1 x (inch)

Stationary glass experiment

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Addition of H₂O to precursor stream

- Stagnate flow reactor experiments (PPG & LBNL studies)
- Change from reaction control to transport control for T > 375C
- Addition of H₂O accelerates the reaction



Deposition mechanism – mass transport

- For N slots with
 - L = the length between inlet and exhaust
 - u = velocity of vapor
 - x = distance from inlet
 - v = velocity of glass

 C_g = concentration of chemistry far from the surface

We can write for the coating thickness h

$$h \propto \frac{N \int_0^L \left(c_g \sqrt{\frac{u}{x}} \right) dx}{v} \propto \frac{N \cdot c_g \cdot u^{1/2} \cdot L^{1/2}}{v}$$

Deposition mechanism – mass transport

But $u \propto \frac{\dot{m_0}}{N \cdot H}$ $c_g \propto \frac{\dot{m_1}}{\dot{m_0}}$

Where

 \dot{m}_0 = total mass flow rate (precursor + carrier gas)

- $\dot{m}_1 =$ precursor flow rate
 - H = coater height above the glass

Such that...

$$h \propto \sqrt{N \cdot L} \cdot \frac{\dot{m_1}}{\sqrt{\dot{m_0}}} \cdot \frac{1}{\sqrt{H}} \cdot \frac{1}{v}$$

Deposition mechanism – mass transport

Similar to the mass transport case

$$J = C_{g}e^{-E/kT}$$

$$h \propto \frac{\dot{m}_1}{\dot{m}_0} \frac{e^{-E/kT}}{T} \frac{L}{\nu}$$

- Low maintenance coatings ("self cleaning")
 - TiO₂
 - Low surface energy when clean – hydrophilic
 - Wide bandgap semiconductor – produces e-h pairs with UV

Sheet Action



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Same deposition mechanism as SnO_2 ?

Design of Experiments – ask what controls thickness

Mass transport controlled• Reaction controlled $\dot{m_1}$ $\frac{\dot{m_1}}{\sqrt{m_0}}$ $\frac{1}{\sqrt{H}}$ $\frac{\sqrt{T}}{v}$ $\frac{\dot{m_1}}{\sqrt{m_0}}$ $\frac{1}{\sqrt{H}}$ $\frac{\sqrt{T}}{v}$ $\frac{\dot{m_1}}{\dot{m_0}}$ $\frac{\dot{m_1}}{\sqrt{m_0}}$ $\frac{1}{\sqrt{H}}$ $\frac{\sqrt{T}}{v}$

•

Thickness	\dot{m}_0	н	т
h_1	\dot{m}_0 (1)	H(1)	T (1)
h_2	$\dot{m}_0(2),\dot{m}_0(2')$	H(2)	T (2)
h_3	\dot{m}_0 (3)	H(3)	T(3)



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TiO2 deposition from titanium isopropoxide

- Online experiments
 - Deposition is mass transport controlled
 - Knowledge of mechanism guides process efficiency improvements

$$\eta = \mathcal{F}(\dot{m}_0, \dot{m}_1, \dot{m}_2, H)$$





Questions

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Materials and Design for Solar Applications

 $TCO \rightarrow Transparent Conductive Oxide$

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Challenges for Solar Applications

Drivers for Technology Development

- Focus on \$/W_p and Levelized Cost of Electricity
- Energy efficient manufacturing
- Device performance
 - Optimize for device and application

Durable

- Long term optical performance
- Mechanically durable

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Glass and Coated Glass for Thin Film PV Maximizing Performance is a Multi-factor Optimization



Current (mA) vs Voltage (V) (measured)

J_{sc}: Light management design

- V_{oc}: TCO materials / interface
- FF: TCO morphology

- Interface morphology is critical to control light path through active layers
- Rough typically used for thin film Si (above)
- Smooth needed for thin film CdTe

Design of High Performance Superstrates TCO Coating Designs

In general electrical and optical properties of the TCO cannot be specified separately



Impact of conductivity on PV performance



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Engineering of the Bulk TCO to Reduce Optical Losses

Root causes of losses

- 1. Intrinsic absorption
- 2. Free carriers

$$\lambda_p = \frac{2\pi c}{\omega_p} = 2\pi c \sqrt{\frac{\varepsilon_o \varepsilon_\infty m^*}{ne^2}}$$

- 3. Bandgap
- Materials engineering and design
 - Film quality
 - Increase Permittivity
 - Increase Mobility
 - Increase Bandgap





Materials Engineering – reducing optical losses

- Alloying of SnO₂ matrix to modify permittivity
- Electrical properties comparable to SnO₂:F
- Optical properties comparable to undoped material



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Light Redirection by Morphology Engineering

Increased optical path length through PV active layer



Morphology Design – Tandem α -Si PV

- What is optimal crystal size for maximizing scattering in region of interest?
 - Small sized
 - Mie scattering
 - SnO₂/Si interface
 Optical indices
 - Ensemble of sizes form of distribution

statistics

Morphology Design Determination of form of Distribution

- Consider an ensemble of grains with distribution G
- Determination of form is difficult in *R* space – map into Fourier
 space

Grain Size Distribution Scales and is Lognormal

Optimization of Grain Size / Morphology Scattering amplitude vs. wavelength for different sizes of scattering features (SnO₂/Si interface)

- Distribution of sizes (lognormal, σ=20% of μ)
- For structures in Si, calculations indicate long length scale features should be ~0.2μm

Red is high scattering Dark green is low scattering

Optical Wavelength (µm)

Interface Design – CdTe

Buffer layers

- Typically *i*-SnO₂ or in the ZnO-SnO₂ system
- Very high resistance (1000+ Ω-cm)

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Device Performance with Buffer Layer

- Device structure
 - 50 nm CdS
 - 850 nm CdTe

Process

- Magnetron sputtering
- Low substrate temp

Results

HRT1 increased efficiency increased process robustness

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Function of the Buffer Layer – Two Hypothesis

- Buffer layer reduces the number of shunts
 - Surface energy of the buffer material changes the CdS growth mode
 - CdS morphology has fewer pinholes for shunts

- Buffer layer modifies the band alignment
 - Material's properties and / or interface states create barriers
 - Barriers reduce Voc of device

Summary

- CVD is effective technique for large area high volume production of low-E coatings that reduce transport of thermal radiation
 - Control of emissivity
 - Color and aesthetics
- CVD can produce TCO coatings for thin film PV applications
 - Engineering of interface roughness and band alignment
 - Materials and stack design for control of electrical and optical properties
- Process and equipment design
 - Robust process and equipment
 - Design of process through basic materials properties
 - Mass transport or reaction control of deposition

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